

Ch 3.4 Div and Curl of a Vector Field

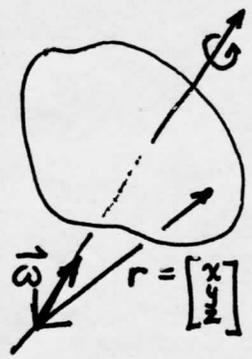
Let $F: \mathcal{U} \rightarrow \mathbb{R}^3$ be a C^1 smooth v.f.

Define $\text{Curl}(F) := \nabla \times F := \det \begin{bmatrix} \hat{i} & \hat{j} & \hat{k} \\ D_x & D_y & D_z \\ F^1 & F^2 & F^3 \end{bmatrix} = \begin{bmatrix} F_y^3 - F_z^2 \\ F_z^1 - F_x^3 \\ F_x^2 - F_y^1 \end{bmatrix}$

P.179 Thm Let $f \in C^2 \Rightarrow \nabla \times (\nabla f) = \vec{0}$

Example of $d^2 = 0$

Pf. $\nabla \times \nabla f = \det \begin{bmatrix} i & j & k \\ D_x & D_y & D_z \\ f_x & f_y & f_z \end{bmatrix} = \begin{bmatrix} f_{yz} - f_{zy} \\ -(f_{xz} - f_{zx}) \\ f_{xy} - f_{yx} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$ by equality of mixed partials (see ch 2.6) \square



Consider a rigid body B rotating about an axis defined by the angular velocity vector $\vec{\omega}$. Then the velocity v.f. for pts on B is given by $\vec{v} = \vec{\omega} \times \vec{r}$. For simplicity, they assume $\vec{\omega} = \begin{bmatrix} 0 \\ 0 \\ \omega \end{bmatrix}$ (along z axis) (see my work in Beer & Johnston VMFE)

What is $\text{Curl}(\vec{v})$? $\vec{v} = \vec{\omega} \times \vec{r} = \begin{vmatrix} i & j & k \\ 0 & 0 & \omega \\ x & y & z \end{vmatrix} = \begin{bmatrix} -\omega y \\ -(\omega x) \\ 0 \end{bmatrix}$

$\text{Curl}(\vec{v}) = \nabla \times \vec{v} = \begin{vmatrix} i & j & k \\ D_x & D_y & D_z \\ -\omega y & \omega x & 0 \end{vmatrix} = \begin{bmatrix} 0 \\ 0 \\ \omega + \omega \end{bmatrix} = 2\vec{\omega}$

Intuitively, $\text{Curl}(F)_x$ measures the rotation of a microscopic paddlewheel in the flow of \vec{F} . $\text{Curl}(F) = 0$ means F is irrotational. This is justified by Stokes Thm in ch 7

Def Divergence $\text{div}(F) := \nabla \cdot F := \sum D_i F^i$

Thm $\text{div}(\text{Curl}(F)) \equiv 0$ i.e. $\nabla \cdot \nabla \times F = 0$

Another example of $d^2 = 0$

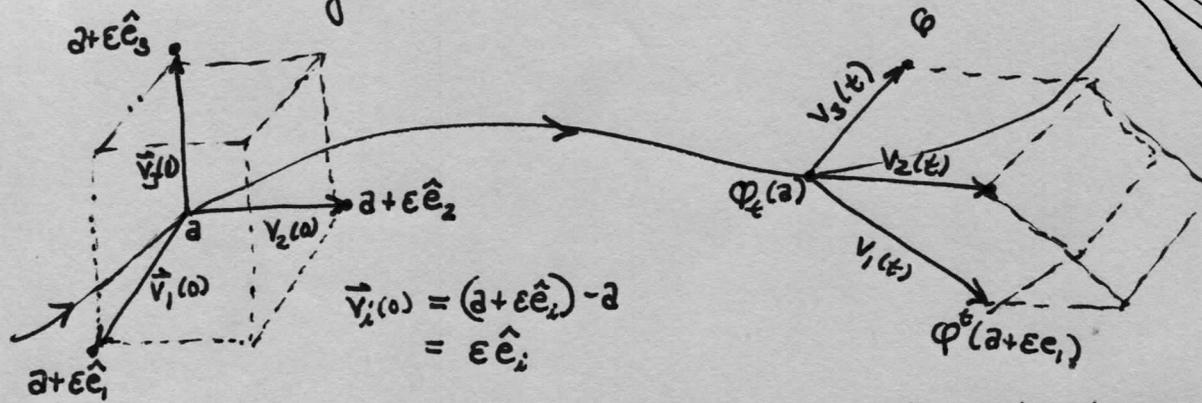
Pf $\nabla \cdot (\nabla \times F) = \nabla \cdot \begin{bmatrix} F_y^3 - F_z^2 \\ F_z^1 - F_x^3 \\ F_x^2 - F_y^1 \end{bmatrix} = F_{xy}^3 - F_{yz}^2 + F_{yz}^1 - F_{yx}^3 + F_{zx}^2 - F_{zy}^1 = 0$ equality of mixed partials \square

If $\text{div}(F) = 0$ we call the flow incompressible. This will be justified shortly.

Laplace operator $\nabla^2 f = \nabla \cdot (\nabla f) = f_{xx} + f_{yy} + f_{zz}$

$\dot{x} = F(x)$ with flow Φ . First we want to explore the relationship between the

Consider a tiny cube with sides parallel to co-ord axes and let it be moved and deformed by the flow.



rate of change of volume of an element of fluid and $\text{div}(F)$ of the ~~flow~~ v.f.

We can approximate the cube at some time t after it has been moved by the flow by the Taylor series approx: the corner pts have been moved

$$\Phi_t(a + \epsilon v) = \Phi_t(a) + D(\Phi_t)_a(\epsilon v) + \mathcal{O}(\epsilon^2)$$

This approx makes this discussion not rigorous, but see the remarks after.

then
$$v_i(t) = \Phi_t(a + \epsilon v_i(t)) - \Phi_t(a) \approx D(\Phi_t)_a(\epsilon v_i(t)) \text{ for } i=1,2,3$$

As the cube moves with the flow, its end pts define a parallelepiped. An expression for the volume of this is $\text{Vol}(t) = V(t) = v_1(t) \cdot [v_2(t) \times v_3(t)]$ triple product

P.184 Thm For such a cube,
$$\frac{V'(0)}{V(0)} = \text{div}(F)_a$$

Pf The idea is that if we calculate $V'(0)$, the divergence $\nabla \cdot F$ falls out.

$$V'(t) = \dot{v}_1(t) \cdot [v_2 \times v_3] + v_1 \cdot [\dot{v}_2 \times v_3] + \dots$$

To see this, note triple prod $a \cdot (b \times c) = \det \begin{bmatrix} a & b & c \\ -a & - & - \\ - & - & - \\ - & - & - \end{bmatrix}$
Thus $= b \cdot (c \times a) = c \cdot (a \times b)$
 $\rightarrow b_2$
 $a \leftarrow c$

Evaluate at $t=0$
 $V'(0)$
By Lemma which appears below

$$\begin{aligned} &= \dot{v}_1 \cdot [v_2 \times v_3] + \dot{v}_2 \cdot [v_3 \times v_1] + \dot{v}_3 \cdot [v_1 \times v_2] \\ &= \dot{v}_1(0) \cdot \underbrace{[\hat{e}_2 \times \hat{e}_3]}_{e_1} + \dot{v}_2(0) \cdot \underbrace{[e_3 \times e_1]}_{e_2} + \dot{v}_3(0) \cdot \underbrace{[e_1 \times e_2]}_{e_3} \\ &= \epsilon^3 [DF_a(e_1)]^T e_1 + \epsilon^3 [DF_a(e_2)]^T e_2 + \epsilon^3 [DF_a(e_3)]^T e_3 \\ &= \epsilon^3 e_1^T DF_a e_1 + \epsilon^3 e_2^T DF_a e_2 + \epsilon^3 e_3^T DF_a e_3 \\ &= \epsilon^3 \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} F_x^1 & F_x^2 & F_x^3 \\ F_y^1 & F_y^2 & F_y^3 \\ F_z^1 & F_z^2 & F_z^3 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} + \dots + \dots \\ &= \epsilon^3 [F_x^1 + F_y^2 + F_z^3] \end{aligned}$$

$$\Rightarrow \frac{V'(0)}{\epsilon^3} = \frac{V'(0)}{V(0)} = (\nabla \cdot F)(a) \quad \text{QED}$$

Now for the lemma \rightarrow

Lemma with our previous approximation,
 $\dot{v}_i(0) = DF_a(v_i(0))$

By \star $\vec{v}_i(t) = \cancel{D_x(\varphi_t)_a(v_0)} D_x(\varphi_t)_a(v_0)$

then $\frac{d}{dt} \vec{v}_i = \frac{d}{dt} D_x(\varphi_t)_a(v_0) = D_x(\dot{\varphi}_t)_a(v_0)$
 \parallel
 $\cancel{D_x(\varphi_t)_a(v_0)} F(\varphi_t)$

Evaluate at $t=0$
 $\varphi_{t=0} = Id$

$= DF_a \cdot D(\varphi_t)_a(v_0)$
 $= DF_a(v_0)$

$\dot{v}_i(0) = DF_a(v_i(0))$

Now we note $v_i(0) = \epsilon \hat{e}_i$ so $\dot{v}_i(0) = \epsilon DF_a(e_i)$ \square

Now let's compare this with some other results:

The definite result (transport thm) is at the end.

\triangle On p.445-446, ch 7.4, MGT use the Divergence thm to show

$(\nabla \cdot F)(x) = \lim_{\rho \rightarrow 0} \frac{\int_{\partial B} \vec{F} \cdot \hat{n} dA}{\text{Vol}(B_\rho)}$ where we have ball $B = B(x, \rho)$

\triangle Arnold's MNOCM^p gives a more general argument. He has a vf $F: \mathbb{R}^n \rightarrow \mathbb{R}^n$ and he ~~also~~ considers the volume of an arb @able set D (not only a parallelepiped).

He defines $\text{Vol}_0(t) := V_D(t) = \int_{\varphi_t(D)} 1 d^n y = \int | \det D\varphi_t^t | d^n x$

CoV Thm
 Apostol, MA
 p.421

Thm $\text{div}(F) = 0 \implies V_D(t) = V_D(0)$ [volume preserving flow]

This uses Key Lemma $V_D'(0) = \int_D \text{div}(F) d^n x$

Step 1 note that for any fixed x , φ_x has the following Taylor expansion about

$t=0$:
 $\varphi_x(t) = \varphi_x(0) + \dot{\varphi}_x(0)(t-0) + \frac{\ddot{\varphi}_x(\xi(x))}{2!}(t-0)^2$

Now allow x to vary and this relationship

$\varphi_t^t(x) = x + F(x)t + h(x)t^2$

$D(\varphi_t^t)_x = I + t DF_x + t^2 Dh_x$

velocity vf of fluid: $\vec{u} = \begin{bmatrix} u \\ v \\ w \end{bmatrix}$

$\vec{\omega} = \nabla \times \vec{u} = \begin{bmatrix} \partial_y w - \partial_z v \\ \partial_z u - \partial_x w \\ \partial_x v - \partial_y u \end{bmatrix}$ vorticity field

claim: clm nbhd of each pt of fluid, $\vec{u} = \text{translation} + \text{deformation} + \text{rigid rotation with rot vector}$
[applies to any vf in \mathbb{R}^3]

$x \in \mathbb{R}^3$
 $y = x+h$

$u(y) = u(x) + \underbrace{x^T D u}_S h + \underbrace{\left(\frac{1}{2}\right) \underbrace{\nabla \otimes \nabla}_W x \cdot h + \theta(h^2)}$

$h^2 = \|h\|^2$

Garrison pool?

Taylor Thm: $u(x+h) = u(x) + D u_x h + \theta(h^2)$

Now define $S_D := \frac{1}{2} [D U + D U^T]$ and $W_S := \frac{1}{2} [D U - D U^T]$

so $D U = S_D + W_S$

co-ord expression for $W_S = \begin{bmatrix} 0 & -\frac{w_2}{m} & \frac{w_1}{m} \\ \frac{w_2}{m} & 0 & -\frac{w_3}{m} \\ -\frac{w_1}{m} & \frac{w_3}{m} & 0 \end{bmatrix}$

then $W_S h = \nabla \times h$

$u(y) = u(x) + \underbrace{(S_D + W_S) h}_{S_D h + \nabla \times h} + \theta(h^2)$

$S_D = Q^T \Lambda_D Q$
[diagonal matrix]

Not flow!

p.20 Since S_D is a symm matrix $S_D = S_D^T$

$S_D h = \text{grad}_h(\varphi(x,h))$ where $\varphi(x,h) = \frac{1}{2} \langle S_D h, h \rangle$

if $b(x) = \langle Ax, x \rangle$
 $Db_x = \langle A$

Avez bilinear
 $b: E_1 \times E_2 \rightarrow F$

$b(a+h) - b(a) = b(a_1, h_2) + b(h_1, a_2) + b(h_1, h_2)$

In M&T VC he says

$\left. \frac{d}{dt} \langle w(t), w(t) \rangle \right|_{t=0} = D F_0^T w_0 + v_0^T D F_0 w_0$
 $= v^T \underbrace{[D F_0 + D F_0^T]}_{2S} w$

We have a v.f. $F: \mathbb{R}^3 \rightarrow \mathbb{R}^3$ and thus $\dot{x} = F(x)$
 we want to show that $\dot{x}(t_0) = (S+W)x(t_0)$, where S is a matrix related to the rate of change of the inner product of 2 vectors under the flow, and W is related to the rotation around the vector $(\nabla \times F)(t_0)$. The discussion is suggestive, not rigorous.

① wlog we take $x_0 = 0$ and we write

$$DF_0 = \underbrace{\frac{1}{2}(DF_0 + DF_0^T)}_S + \underbrace{\frac{1}{2}(DF_0 - DF_0^T)}_W$$

"deformation matrix" "rotation matrix"

② First, let's work on the W piece. We need a Lemma, which is the book's Thm 4 p. 187 [I'm not going to phrase it as a lemma]

Given a fixed vector w ,

The linear map $V: \mathbb{R}^3 \rightarrow \mathbb{R}^3$ has the matrix

$$y \mapsto w \times y \quad \begin{bmatrix} 0 & -w_3 & w_2 \\ w_3 & 0 & -w_1 \\ -w_2 & w_1 & 0 \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \\ y_3 \end{bmatrix}$$

and thus, the expression for V as a linear v.f. is

$$\dot{y} = By$$

if we choose the basis for \mathbb{R}^3 so that $\vec{w} = \begin{bmatrix} 0 \\ 0 \\ \omega \end{bmatrix}$ B ← we can certainly accomplish this by a rotation i.e. a COB by an o.b. matrix Q

Then, magically, B is in ~~block~~ block Jordan Normal form and $\det Q = +1$
 thus we can explicitly write down the flow:

$$\dot{y} = By = \begin{bmatrix} 0 & -\omega & 0 \\ \omega & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x \\ y \\ z \end{bmatrix} \Rightarrow y(t) = e^{Bt} y_0 = \begin{bmatrix} \cos(\omega t) & -\sin(\omega t) & 0 \\ \sin(\omega t) & \cos(\omega t) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x_0 \\ y_0 \\ z_0 \end{bmatrix}$$

It is the same circular flow!
 We just rotate all of \mathbb{R}^3 back so that \vec{w} is in its orig direction.

and we see this flow is a circular rotation around the z axis.
 Hence in the orig basis, the flow is some kind of a rotation about some axis.

Cont'd →

③ Now observe that $W = \frac{1}{2} (DF_0 - DF_0^T)$ has the form of a "B" for $\vec{w} = (\nabla \times F)(\omega)$.

$$\begin{aligned} \frac{1}{2} (DF_0 - DF_0^T) &= \frac{1}{2} \begin{bmatrix} 0 & \left(\frac{\partial F^1}{\partial y} - \frac{\partial F^2}{\partial x}\right) & \left(\frac{\partial F^1}{\partial z} - \frac{\partial F^3}{\partial x}\right) \\ \left(\frac{\partial F^2}{\partial x} - \frac{\partial F^1}{\partial y}\right) & 0 & \left(\frac{\partial F^2}{\partial z} - \frac{\partial F^3}{\partial y}\right) \\ \left(\frac{\partial F^3}{\partial x} - \frac{\partial F^1}{\partial z}\right) & \left(\frac{\partial F^3}{\partial y} - \frac{\partial F^2}{\partial z}\right) & 0 \end{bmatrix} \\ &= \begin{bmatrix} 0 & -(\nabla \times F)^{\textcircled{3}} & (\nabla \times F)^{\textcircled{2}} \\ (\nabla \times F)^{\textcircled{3}} & 0 & -(\nabla \times F)^{\textcircled{1}} \\ -(\nabla \times F)^{\textcircled{2}} & (\nabla \times F)^{\textcircled{1}} & 0 \end{bmatrix} \end{aligned}$$

④ Now we show that the S piece falls out when we consider the rate of change of the inner product of 2 vectors carried by the flow. Note that we don't show that W is wholly responsible for rotation and S for deformation; that may be true but we don't show it.

See for any missing details.

Let $\vec{v}(t) = D(\varphi^t)_0(v)$ $\vec{w}(t) = D(\varphi^t)_0(w)$

$$\begin{aligned} \left. \frac{d}{dt} (v(t) \cdot w(t)) \right|_{t=0} &= \dot{v}(0)^T w(0) + v(0)^T \dot{w}(0) \\ &= (DF_0(v))^T w + v^T DF_0(w) \\ &= (Av)^T w + v^T Aw \\ &= v^T A^T w + v^T Aw \\ &= v^T \underbrace{[A^T + A]}_{\text{This is } 2S} w \end{aligned}$$

~~See for any missing details~~

